



Aerospace Engineering Seoul National University



2020년 한국연소학회 춘추계 통합 온라인 학술대회

희박 예혼합 저선회 연소기의 화염전달함수 수치해석

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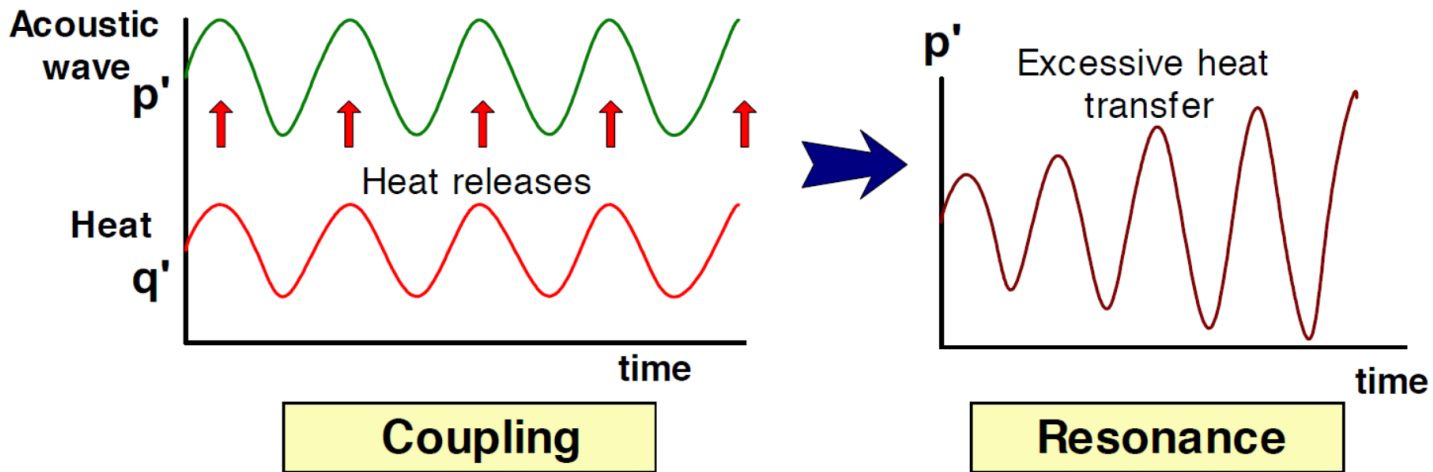
2020. 09. 24.

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Introduction : Thermoacoustic instability

- A resonant phenomena as a result of mutual coupling between acoustic wave and unsteady heat release perturbation from the combustion process
- It could be accompanied by a large pressure fluctuation and pose a threat to system safety
- The predictive capability of combustion instability is required to design the combustion system



Introduction : FTF

- **Flame Transfer Function**

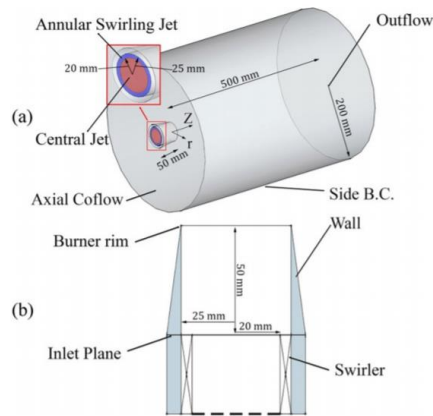
A flame transfer function describes the change in the rate of heat release in response to perturbations in the inlet flow as a function of frequency.

$$FTF(f) = \frac{q'(f)/\bar{q}}{u'(f)/\bar{u}}$$

A measure of representing flame response to acoustic disturbance

Introduction : Reference research

- M. Shahsavari et al., 27th ICDERS. (2019)
- FTF simulation In low-swirl burner



Low swirl configuration of Lund Univ.

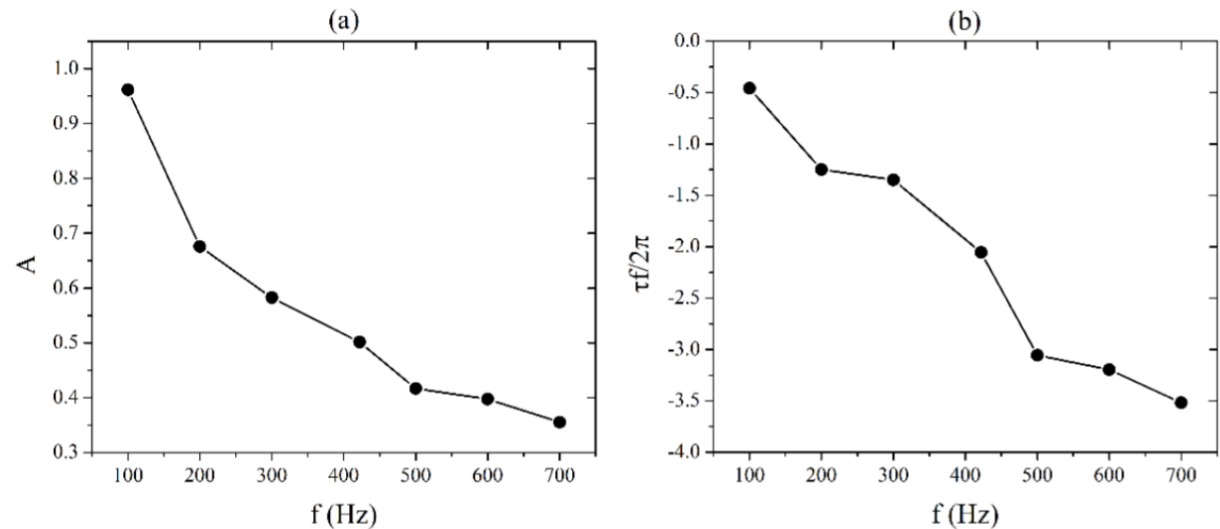


Figure 7. (a) Frequency and (b) phase of the low swirl flame response

Introduction : Reference research

- H. Jegal et al., Proc. Combust. Inst. (2020)
- FTF experiment In low-swirl burner

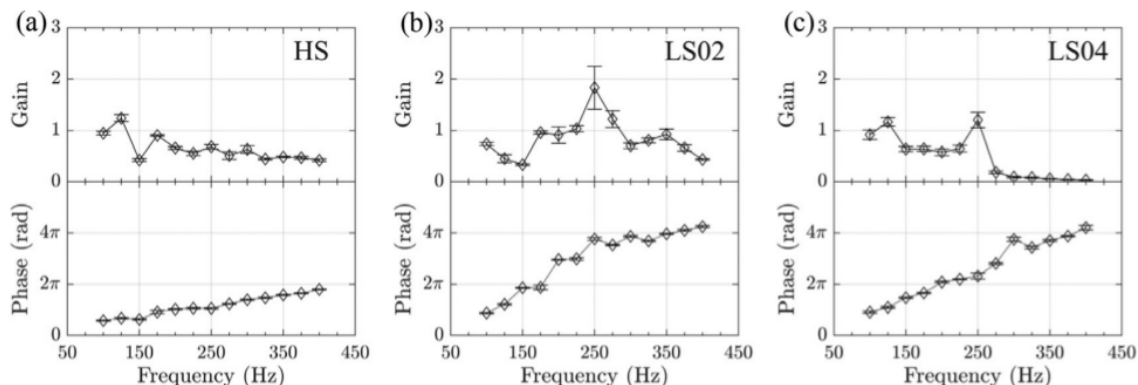
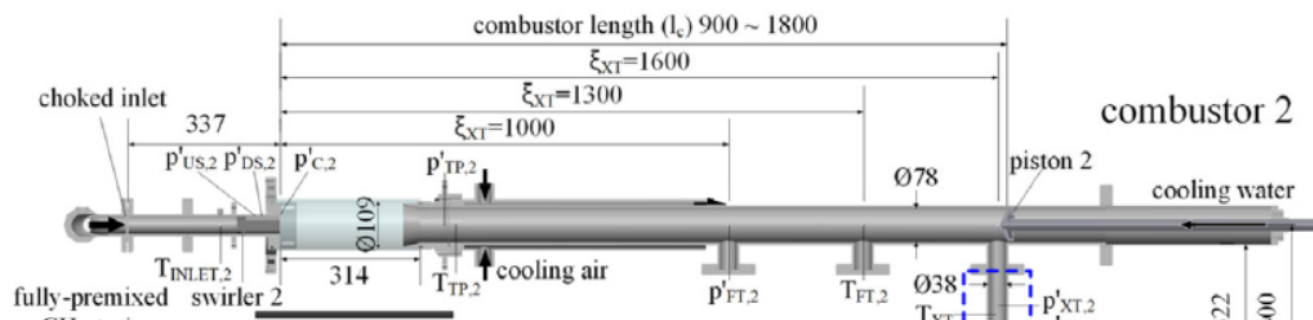
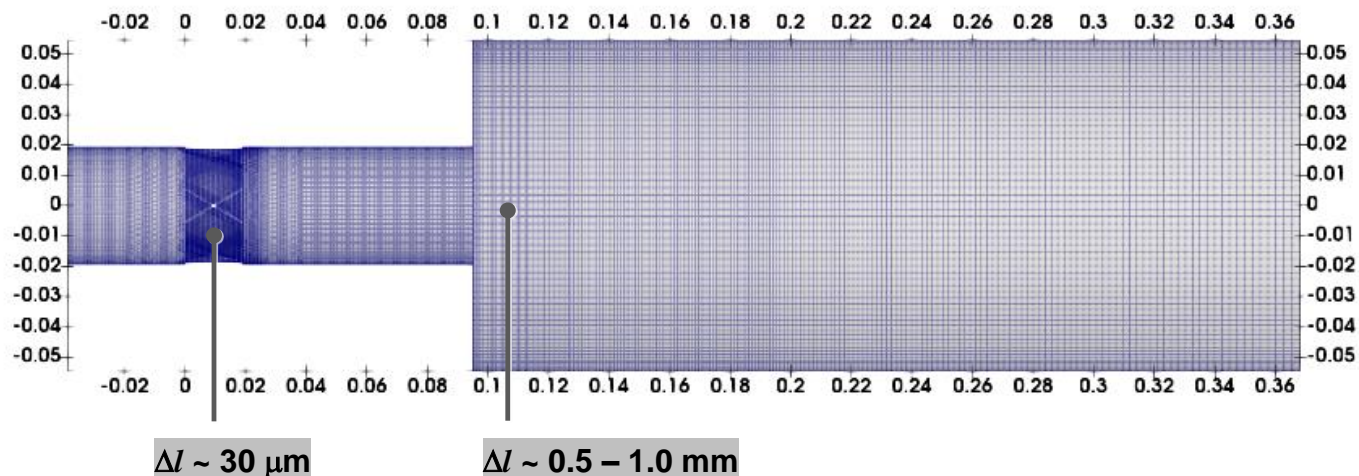


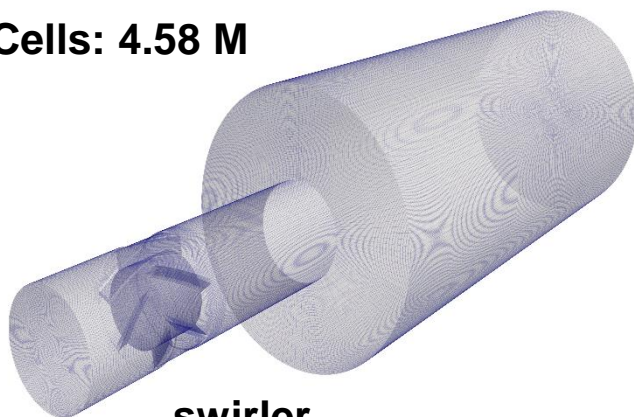
Fig. 4. Flame transfer functions (FTF) of the HS, LS02, and LS04 flames at $\phi_1 = \phi_2 = 0.65$. The FTF is defined as the ratio of the normalized heat-release-rate fluctuations (q'/\bar{q}) to the normalized inlet velocity fluctuations (u'/\bar{u}).

Numerical Method

- Computational domain



Cells: 4.58 M



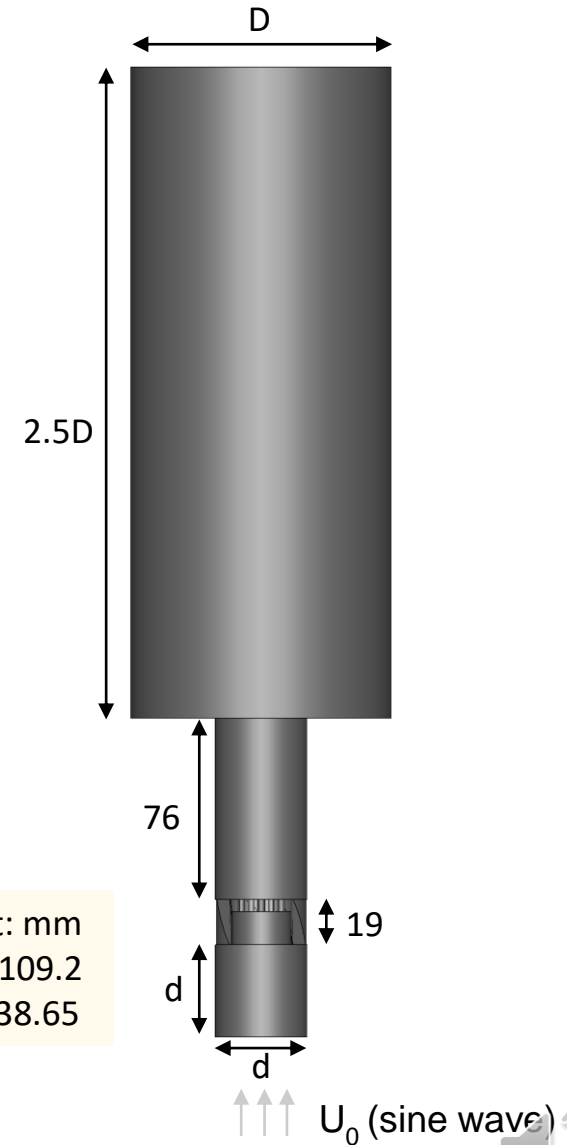
swirler



Numerical Method

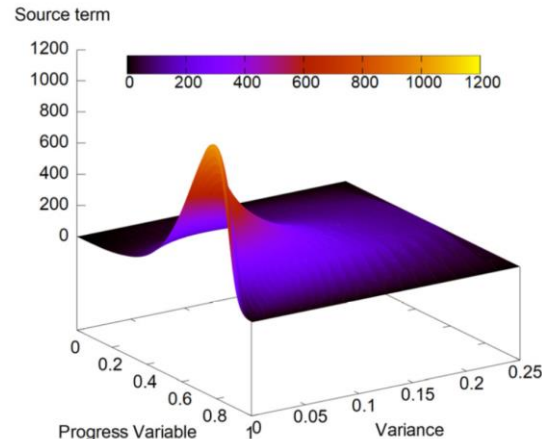
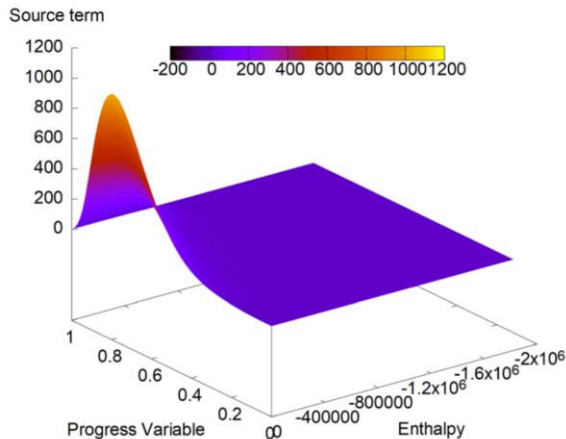
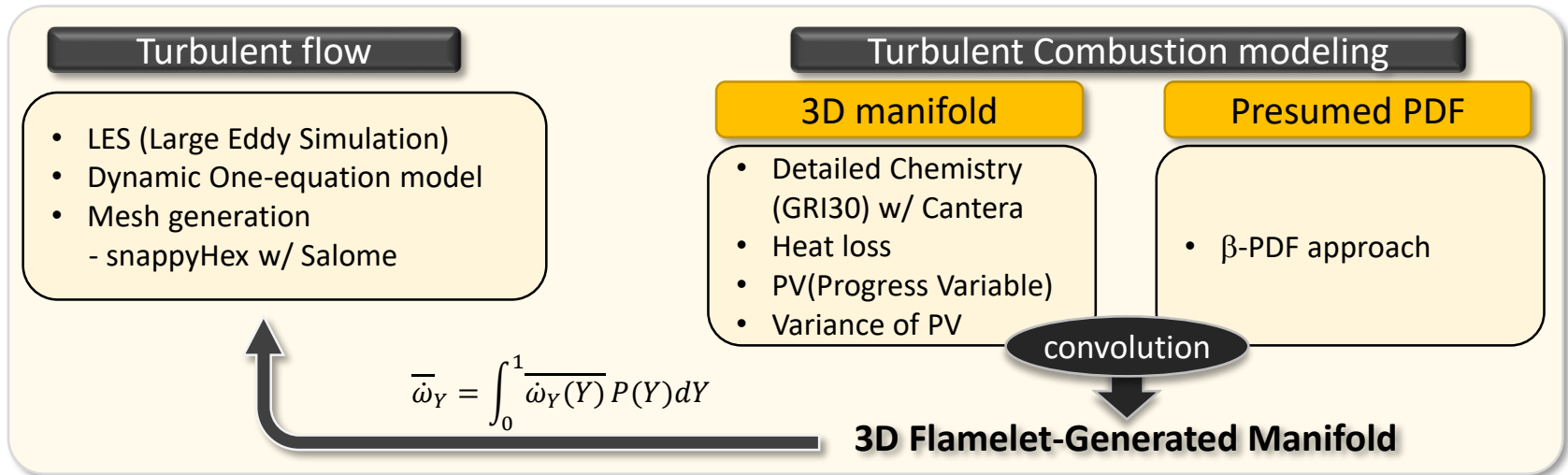
- Reactant: **premixed methane/air**
- Equivalence ratio: **0.65**
- Outlet pressure: **1 atm**
- Inlet temperature: **473 K**
- Inlet mean velocity: **11.48 m/s**

- Excitation
 - **sine wave**
 - frequency: **100 ~ 400 Hz**
 - amplitude: **10 %**



Numerical Method

- FGM (Flamelet Generated Manifold)



Numerical Method

- **Non-reflecting Boundary Conditions**

Advection equation

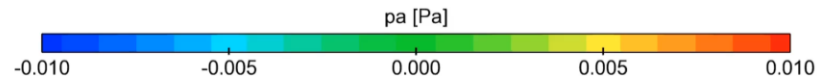
$$\frac{D\phi}{Dt} = \frac{\partial\phi}{\partial t} + \mathbf{U} \cdot \nabla\phi = 0$$

$$\frac{D\phi}{Dt} \approx \frac{\partial\phi}{\partial t} + U_n \cdot \frac{\partial\phi}{\partial \mathbf{n}} = 0$$

Advection speed :

$$U_n = u_n$$

Reflecting B.C.



Non- Reflecting B.C.



Source: <https://youtu.be/J-52qLLDku4>

Results

- Comparison injector

HS vs LS02

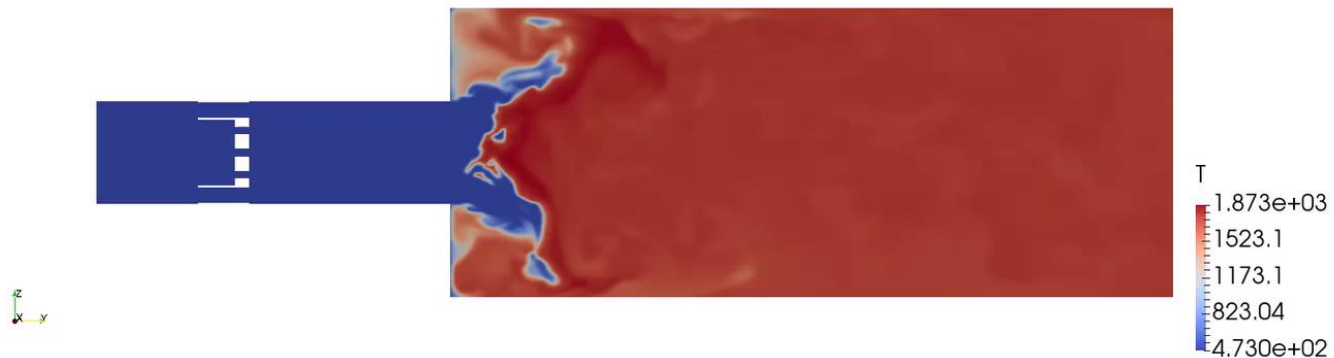
Time: 0.2000 s

HS



Time: 0.2000 s

LS02



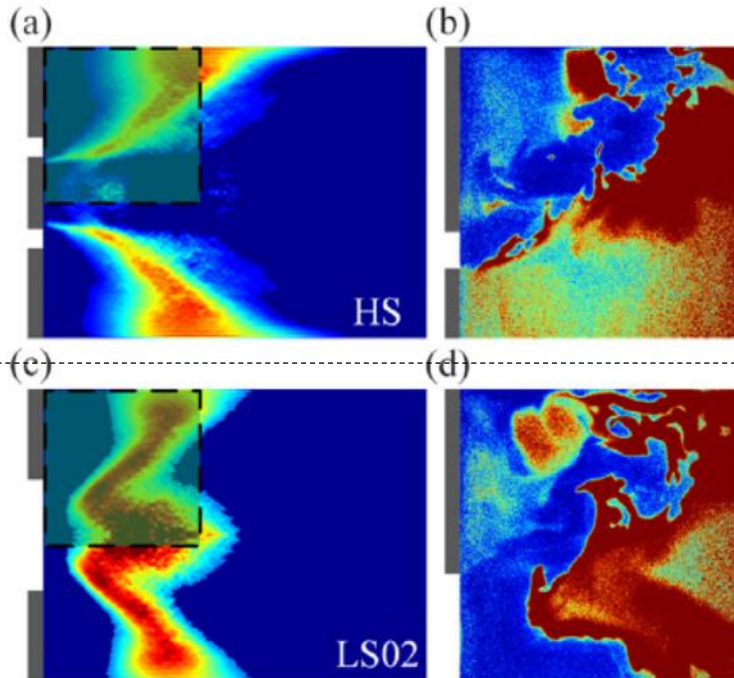
Results

- Comparison injector

Previous experiment

CH* chemilumi.

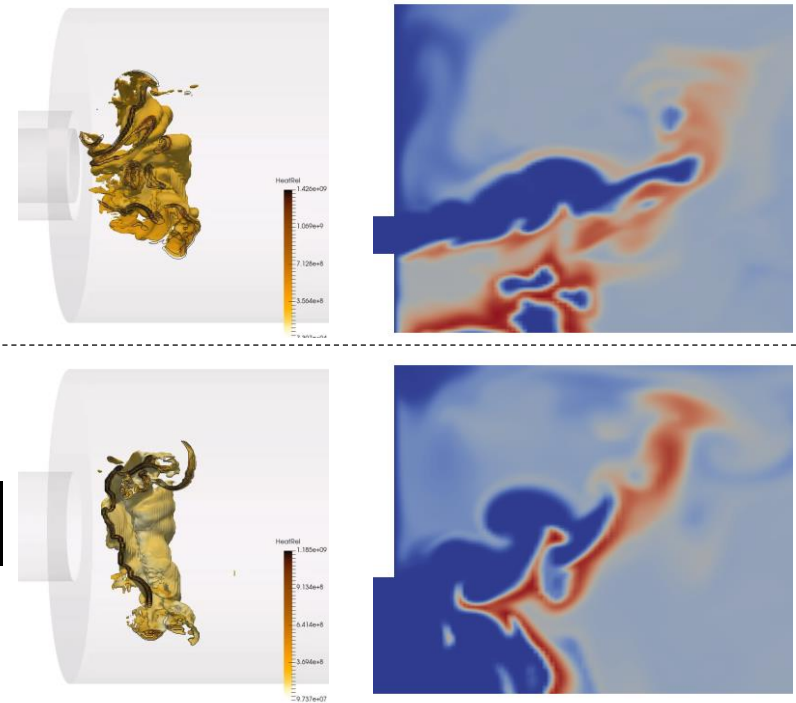
OH PLIF



Present simulation

CH

OH



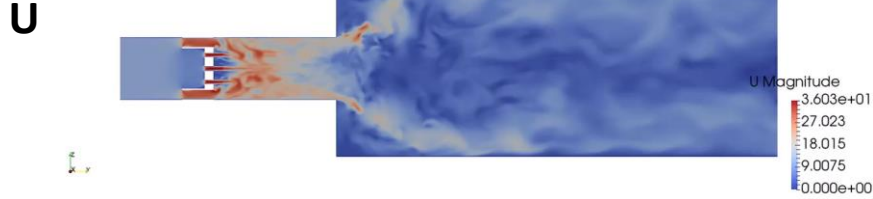
Results

- Comparison frequency

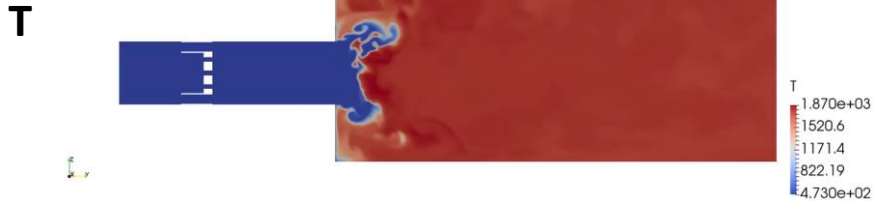
LS02

0Hz

Time: 0.2000 s



Time: 0.2000 s

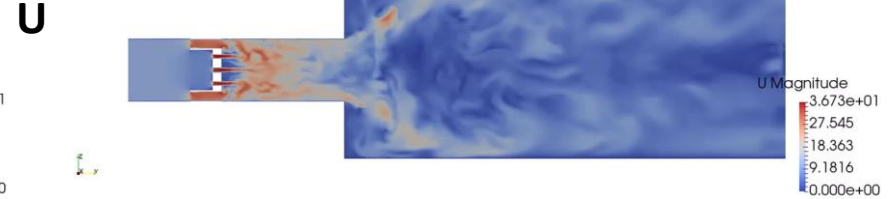


Time: 0.2000 s

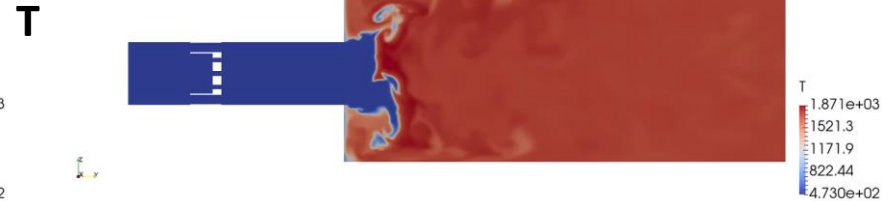


250Hz

Time: 0.2000 s



Time: 0.2000 s



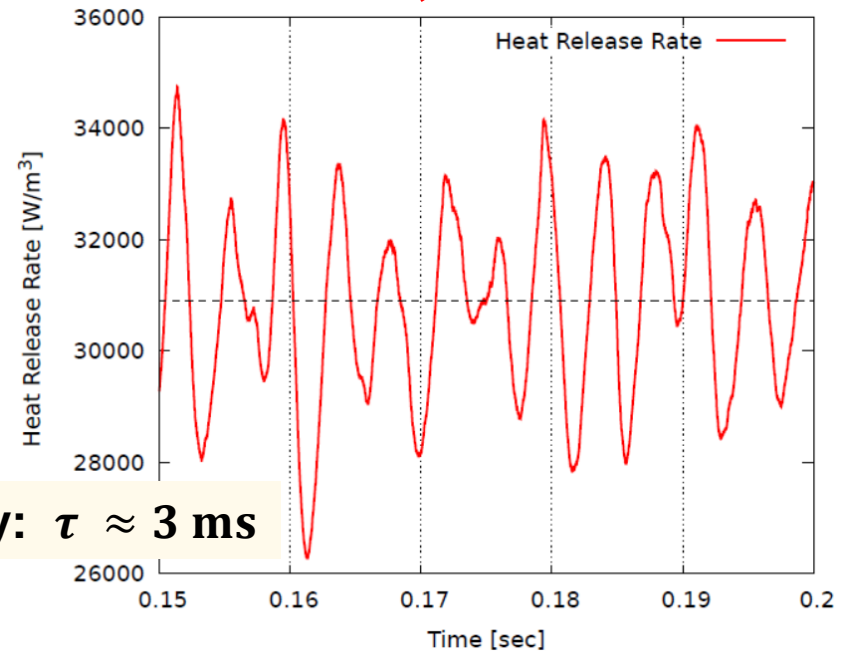
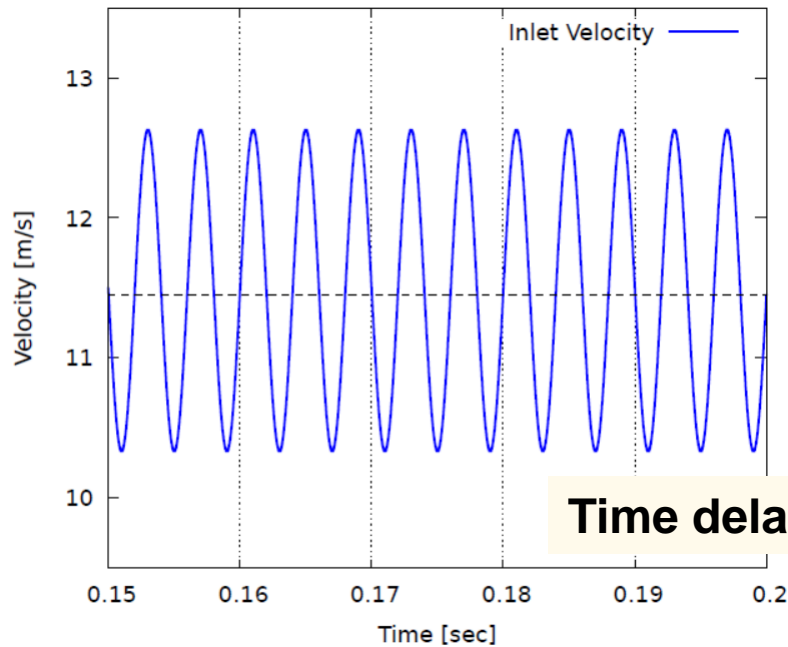
Time: 0.2000 s



Results

- Acquisition FTF

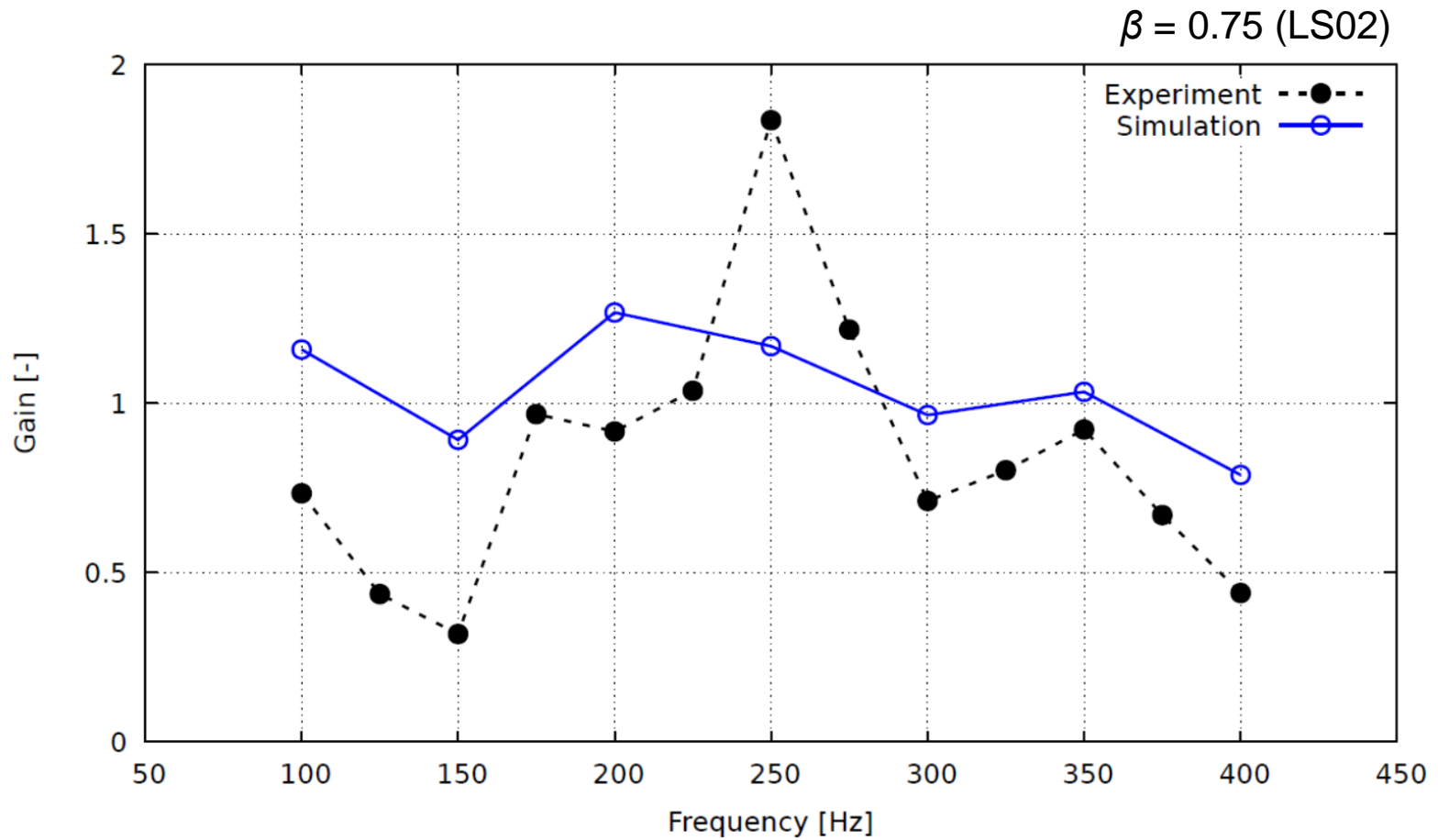
- LS02, 250Hz



Time delay: $\tau \approx 3$ ms

Results

- Low swirl injector - FTF



Conclusion & Future work

- **Velocity excitation** and **non-reflecting** boundary conditions and **FGM** technique were applied.
- **Attached flame** of HS and **lifted flame** of LS were observed.
- The FTF results of simulation on LS02 **tend to be similar** to the **experimental** results.
- Simulation of HS and LS04 will be performed.

Thank you for your attention.

